

**Basis**

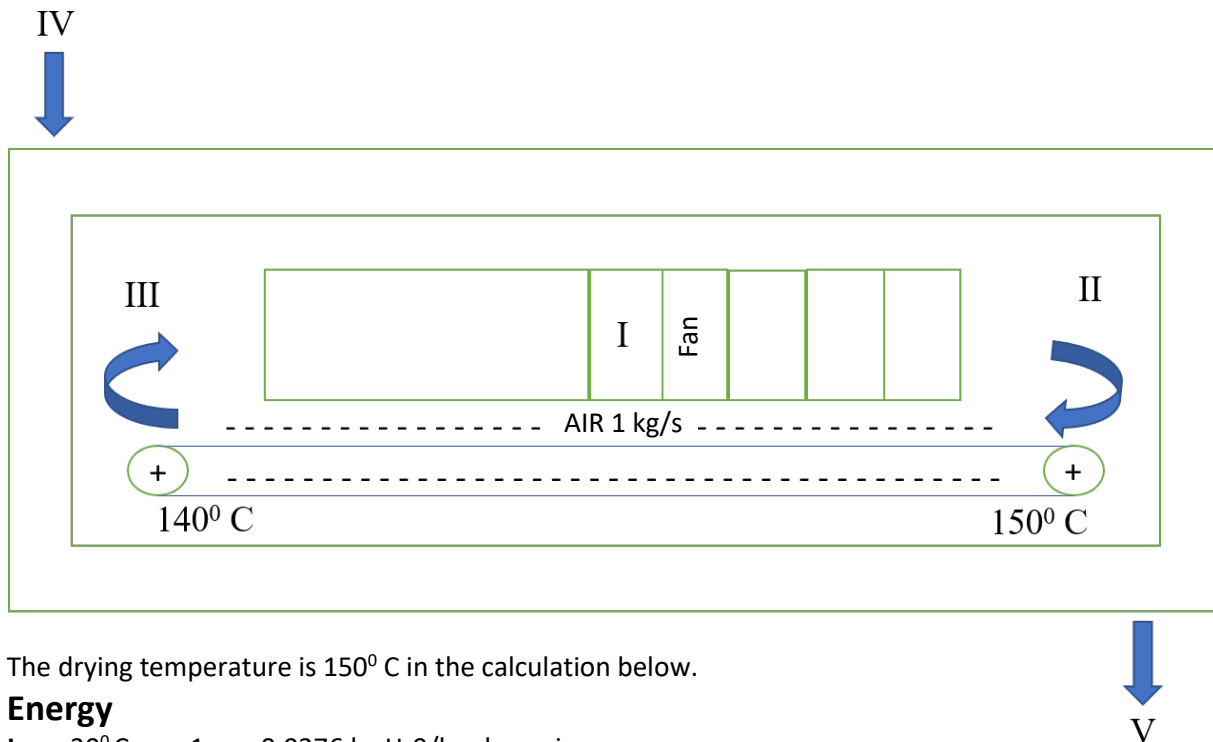
50 000 ton (t.) FAB/in/year(y) 65% DM

Product out: 85% DM

Uptime: 5060 h/y

Calculation $FAB\ in/s = 50\ 000/5060 \times 3600 = 2,745\ kg/s$ $100\%\ DM/y = 32\ 500\ t./y$ $Product\ out,\ 85\%\ DM/y = 38\ 235\ t./y$ $Product\ out,\ 85\%\ DM/h = 7.556\ t./h$ $Product\ out,\ 85\%\ DM/s = 2.099\ kg/s$ $Dehumidification/y = 50\ 000 - 38\ 235 = 11765\ t./y$ $Dehumidification/h = 11\ 765/5060 = 2.325\ t./h$ $Dehumidification/s = 2325/3600 = 0,646\ kg/s$ **Water balance** $100\%\ H_2O/s = 0.35 \times 50\ 000/5060 \times 3600 \cong 0.961\ kg/s$ $15\%\ H_2O\ | product\ out/s = 0.15 \times 2.099 \cong 0.315\ kg/s$ $Condensate = 0.961 - 0.315 = 0.646\ kg/s$

Dehumidification is equal to the condensate, as it should be



The drying temperature is 150° C in the calculation below.

Energy

I. 30° C, $\phi = 1$, $x = 0.0276$ kg H₂O/kg clean air.

$$i_1 = 30 \times 1.005 + 0.0276(2500 + 30 \times 1.86) = 101 \text{ kJ/kg clean air}$$

II. 150° C, $x = 0.0276$ /kg clean air

$$i_2 = 150 \times 1.005 + 0.0276(2500 + 150 \times 1.86) \cong 227 \text{ kJ/kg clean air}$$

III. 140° C, $x = 0.0276 + 0.646 = 0.674$ /kg clean air

$$i_3 = 140 \times 1.005 + 0.674(2500 + 140 \times 1.86) \cong 2000 \text{ kJ/kg clean air}$$

IV. Added energy in FAB in: $2.745 \times 3 \times 15 \cong 124$ kJ/s

V. Abducted energy in product out: $2.099 \times 1.8 \times 50 \cong 189$ kJ/s

VI. Heat leakage: $200 \times 120 \times 0.5 \cong 10$ kW

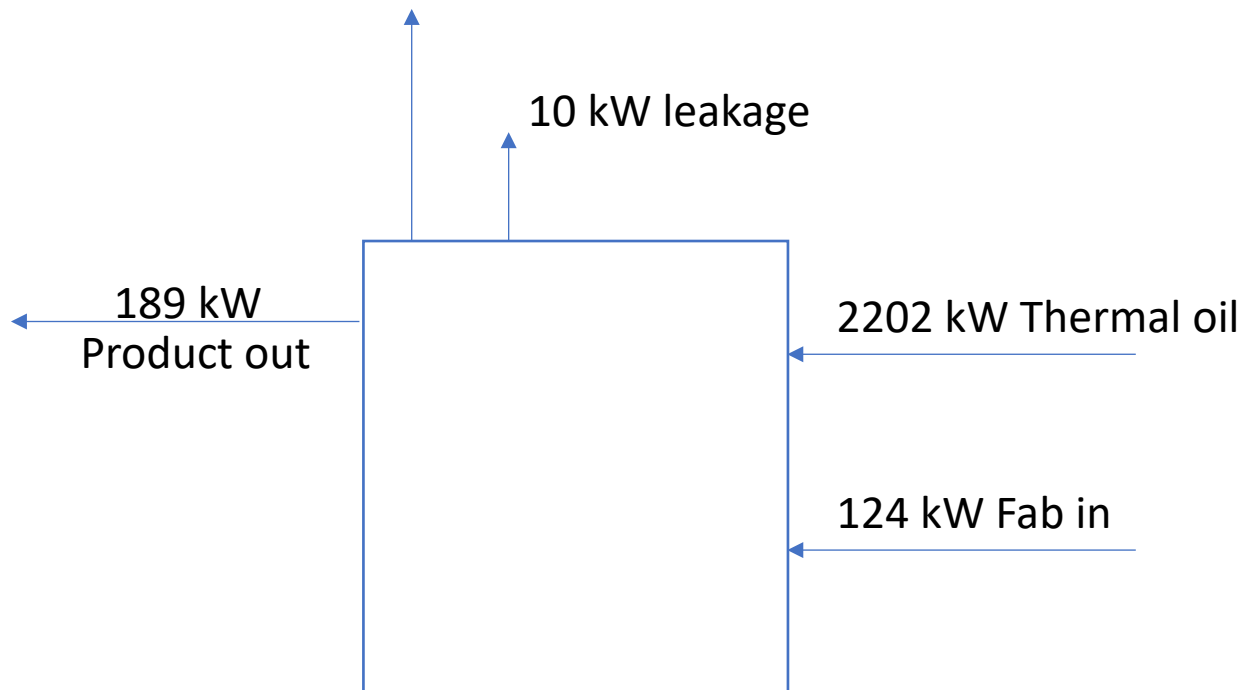
Energy consumption:

$$\text{III} - \text{I} + \text{II} - \text{IV} + \text{V} + \text{VI} =$$

$$2000 - 100 + 227 - 124 + 189 + 10 = 2202 \text{ kJ/s} = 2202 \text{ kW}$$

**Energy Balance**

Dehumidification: III - I + II = 2127 kW



If we can use the condensation energy:

Condensate 0.646 kg/s

Temperature: $\sim 50^\circ\text{C}$

Condensate enthalpy: 2382 kJ/kg

Condensation effect:

 $2382 \times 0.646 \cong 1539\text{ kW}$

Can be used to heat FAB in.

Mass balance